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(54) **Circuit arrangement**

Schaltungsanordnung

Circuit

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Description

The invention relates to a circuit arrangement for operating a high-pressure discharge lamp provided with

- a ballast circuit for generating a current through the high-pressure discharge lamp from a supply voltage,
- first means for controlling a power consumed by the high-pressure discharge lamp,
- second means for influencing a run-up behaviour of the high-pressure discharge lamp and comprising third means for controlling the luminous flux of the high-pressure discharge lamp.

Such a circuit arrangement is known from the International Patent Application WO 87/01553 laid open to public inspection.

When the known circuit arrangement is used to operate the high-pressure discharge lamp, to be called the lamp hereinafter, the luminous flux of the lamp is subject to a comparatively great change during the run-up. The duration of the run-up, however, is often of the order of 10 seconds.

This comparatively great change in the luminous flux during a comparatively long time is felt to be undesirable in many applications.

The invention has for its object to provide a circuit arrangement by which the luminous flux of a lamp operated by means of this circuit arrangement is controllable at the same substantially constant level as the level at which the luminous flux is maintained during stationary lamp operation at least during the major portion of the run-up phase of the lamps

A circuit arrangement according to the invention is for this purpose characterized in that the third means comprise a light sensor coupled with a control circuit for controlling the power supplied to the high-pressure discharge lamp in such a way that the luminous flux of the high-pressure discharge lamp remains at a substantially constant level and in that the second means further comprise fourth means for the automatic activation of the first means after the run-up of the high-pressure discharge lamp.

During operation of a circuit arrangement according to the invention, the third means are active and the first means are inactive immediately after lamp ignition, and the lamp has a comparatively low luminous efficacy. This comparatively low luminous efficacy is the result of the fact that the temperature of the lamp is considerably lower than the stationary operating temperature. At this considerably lower temperature, the composition of the plasma of the lamp differs from the composition at the stationary operating temperature. During the run-up of the lamp, the temperature of the lamp and the luminous efficacy increase, while the composition of the plasma of the lamp changes. The lamp run-up is completed when the temperature of the lamp, the luminous efficacy

and the composition of the plasma of the lamp have become substantially constant. The third means are capable of controlling the luminous flux of the lamp at a substantially constant value during substantially the entire duration of the lamp run-up. Circuit arrangements for operating the lamp, however, are in practice often provided with limitation means for limiting the power consumed by the lamp in order to prevent damage to the lamp and the circuit arrangement. As a result of the operation of these limitation means, which imply a restriction of the operation of the third means, the luminous flux is lower than a desired level during a first comparatively short initial phase of the run-up phase of the lamp, in which the luminous efficacy of the lamp assumes comparatively low values. After the first comparatively short initial phase of the run-up of the lamp, the third means control the luminous flux of the lamp for the further duration of the run-up at a substantially constant level.

After the run-up of the lamp, the fourth means activate the first means, so that no longer the luminous flux of the lamp, but the electric power consumed by the lamp is kept substantially constant. If the third means are calibrated in relation to the first means, the luminous flux of a lamp operated on the circuit arrangement is at the same substantially constant level as during stationary lamp operation after the first comparatively short initial phase of the run-up of the lamp. The application possibilities of the lamp are considerably increased by this.

It should be noted that the use of a circuit arrangement by which the luminous flux of the lamp is kept substantially constant both during the run-up and during stationary operation also provides a solution to the set problem. An important disadvantage of the use of such a circuit arrangement, however, is that, if the luminous efficacy of the lamp decreases owing to, for example, ageing, the electric power consumed by the lamp increases also during stationary lamp operation. The life of the lamp is considerably shortened by this.

It should also be noted that US Patent 4,190,795 discloses a circuit arrangement for operating a high-pressure mercury discharge lamp, which circuit arrangement is provided with means for keeping the luminous flux of the high-pressure mercury discharge lamp substantially constant and also with means for keeping the power consumed by the high-pressure mercury discharge lamp substantially constant. The high-pressure mercury discharge lamp operated on said circuit arrangement is meant to be used in photolithographic processes. The means for keeping the power consumed by the high-pressure mercury discharge lamp substantially constant are only meant to keep the high-pressure mercury discharge lamp in an operating condition in which the luminous flux of the high-pressure mercury discharge lamp is comparatively low, when the means for keeping the luminous flux substantially constant are not active, for example, between two successive photolithographic process steps. During a photolithographic process step, the luminous flux of the lamp is compar-

atively high. In addition, the said circuit arrangement lacks means for automatic activation of the means for keeping the power consumed by the high-pressure mercury discharge lamp substantially constant after the run-up of the high-pressure mercury discharge lamp. The circuit arrangement described in this Patent is not suitable for controlling the run-up behaviour of a high-pressure discharge lamp for these reasons.

The moment at which the fourth means activate the first means in a circuit arrangement according to the invention may, for example, depend on a lamp parameter which changes strongly during the run-up of the lamp, such as, for example, lamp current, lamp voltage, or the temperature at a certain area of the lamp. However, since the time duration of the run-up of each lamp of a certain type and associated power lies within comparatively narrow limits, it is advantageous to provide the fourth means with a timer circuit which initiates the activation of the first means by the generation of a signal whenever a fixed time interval has elapsed after lamp ignition. It is possible with such a timer circuit to control the moment at which the first means are activated in a simple and reliable manner.

As was noted above, it is possible through a calibration of the third means in relation to the first means to prevent the luminous flux being subject to a major change when the first means are activated after the run-up of the lamp. If, however, for example owing to ageing, the luminous efficacy of the lamp changes or a light sensor forming part of the third means becomes polluted and as a result gives a different signal as a measure for this luminous flux, the calibration shows drift. As a result of this drift, there will be a change in the luminous flux from a first substantially constant level to a second substantially constant level when the first means are activated after the run-up of the lamp. This can be prevented in that the calibration is carried out automatically at regular intervals and in that the result of the calibration is stored in a memory in which this result remains stored also when the lamp is not ignited. It is achieved in this way that, in spite of the ageing of the circuit arrangement and of the lamp operated on the circuit arrangement, the luminous flux of the lamp shows substantially no change when the first means are activated after the run-up of the lamp.

Such a memory may be composed in a simple and reliable manner from a digital memory element, a digital/analog converter, and an analog/digital converter.

Embodiments of the invention will be explained in more detail with reference to a drawing, in which

Fig. 1 is a diagram of an embodiment of a circuit arrangement according to the invention;
Fig. 2 is a diagram of a further embodiment of a circuit arrangement according to the invention; and
Fig. 3 is a diagram of an embodiment of a memory for use in a circuit arrangement as shown in Figs. 1 and 2.

In Fig. 1, VI denotes a ballast circuit for operating a discharge lamp by means of a current generated from a supply voltage. K1 and K2 are input terminals of the ballast circuit VI for connection to a supply voltage source. A discharge lamp La is coupled to output terminals of the ballast circuit VI. In this embodiment, means I for controlling the power consumed by the discharge lamp are formed by control circuit 2, multiplier circuit 3 for generating a signal which is a measure for the power consumed by the lamp, and differential amplifier 4. Light sensor SE, differential amplifier 5, control circuit 2, and memory 7 together form means III for controlling the luminous flux of the lamp. Timer circuit 6 and switching element S1 form means IV for automatic activation of the means I after the run-up of the lamp. Timer circuit 6 switching element S2, memory 7, and sensor SE form calibration means for automatic calibration of the means III in relation to the means I. Inputs of the multiplier circuit 3 are coupled to the output terminals of the ballast circuit VI. An output of the multiplier circuit 3 is connected to an input of differential amplifier 4. During operation of the circuit arrangement, a further input 10 of differential amplifier 4 is connected to a substantially constant reference voltage which is a measure for a desired value of the power consumed by the lamp. An output of differential amplifier 4 is connected to an input of control circuit 2 through switching element S1. An output of control circuit 2 is connected to an input of ballast circuit VI. An output of light sensor SE is connected to an input of differential amplifier 5. The output of light sensor SE is also connected to an input of memory 7 through switching element S2. An output of memory 7 is connected to a further input of differential amplifier 5. An output of differential amplifier 5 is connected to switching element S1. An output of timer circuit 6 is connected to a control electrode of switching element S1, to a control electrode of switching element S2, and to a further input of memory 7. Both the switching element S1 and the switching element S2 are either in a first state or in a second state. If switching element S1 is in the first state, switching element S2 is also in the first state and vice versa. The same is true for the second state. In the first state, switching element S1 connects the output of differential amplifier 5 to the input of control circuit 2, and switching element S1 breaks the connection between the output of differential amplifier 4 and the input of control circuit 2. In the first state, switching element S2 breaks the connection between the output of light sensor SE and the input of memory 7. In the second state, switching element S1 breaks the connection between the output of differential amplifier 5 and the input of control circuit 2, and connects the output of differential amplifier 4 to the input of control circuit 2. The output of light sensor SE is connected to the input of memory 7 by switching element S2 when the latter is in the second state.

The operation of the circuit arrangement described is as follows.

When a supply voltage source is connected to the

input terminals K1 and K2, the ballast circuit generates a current on which the lamp La is operated. After the circuit arrangement has been made operational and the lamp has been ignited, the switching elements S1 and S2 are in the first state, so that the means III for controlling the luminous flux of the lamp are active since the output of differential amplifier 5 is connected to the input of the control circuit 2. The connection between the output of differential amplifier 4 and the input of control circuit 2 is broken, so that the means I are inactive. Immediately after lamp ignition, the luminous flux is lower than the desired value during a first, comparatively short initial phase. To prevent an excessive power being consumed by the lamp as a result of this during this first comparatively short initial phase, the circuit arrangement is provided with means, not shown in Fig. 1, for limiting the power consumed by the lamp. At the end of the first, comparatively short initial phase, the luminous flux of the lamp has risen to substantially the desired value. This desired value is determined by the signal present at the output of memory 7, which is a measure for the luminous flux of the lamp during stationary lamp operation. The signal at the output of memory 7 is compared with the signal at the output of the light sensor SE by differential amplifier 5. The signal at the output of differential amplifier 5 drives the control circuit 2. The control circuit 2 controls the power supplied to the lamp La by the ballast circuit in such a way that the luminous flux of the lamp remains constant. It is found in practice that the power supplied to the lamp during the run-up of the lamp decreases continually if the luminous flux remains substantially constant. Depending on the construction of the ballast circuit, the control circuit 2 may control the power supplied to the lamp, for example, by controlling the frequency of the current through the lamp.

A fixed time interval after lamp ignition, the timer circuit 6 switches both the switching element S1 and the switching element S2 to the second state and activates the input of memory 7 through the further input of memory 7. The fixed time interval is so chosen that it is at least equal to the time duration required for the run-up of the lamp La in question. The means I are activated in the second state of the switching elements in that the output of differential amplifier 4 is connected to the input of control circuit 2; means III are rendered inactive in that the connection between the output of differential amplifier 5 and the input of control circuit 2 is broken. A signal which is a measure for the power consumed by the lamp is present at the output of multiplier circuit 3. This signal is compared with the substantially constant reference signal present at input 10 by differential amplifier 4. The signal at the output of differential amplifier 4 drives the control circuit 2 in such a way that the power consumed by the lamp is kept substantially constant at a desired value which is dependent on the substantially constant reference signal.

Since switching element S2 is switched to the second state, the output of light sensor SE is connected to

the input of memory 7. Since this input is activated by the timer circuit 6 through the further input of memory 7, the instantaneous value of the signal at the output of the light sensor SE is stored in the memory. Since the signal at the output of light sensor SE is a measure for the luminous flux of the lamp during stationary lamp operation, means I being active, the storage of the instantaneous value of the signal applied to the input of memory 7 means that the means III are calibrated in relation to the means I, so that the signal at the output of light sensor SE serves as a calibration signal. When the switching element S2 is in the first state, there is no signal at the input of memory 7 and the input of memory 7 is not yet activated through the further input by timer circuit 6. In this state the input of the memory is passive and the memory holds on to the value last stored. This value last stored is also maintained when the circuit arrangement is not operational. The memory 7 is for this purpose provided with a further supply voltage source, for example, in the form of a battery. The luminous flux of a lamp operated by means of a circuit arrangement as shown in Fig. 1 is substantially equal to the luminous flux during stationary lamp operation during the run-up, independent of ageing or pollution of the lamp or the light sensor.

In Fig. 2, circuit components corresponding to circuit components of the circuit arrangement shown in Fig. 1 are correspondingly referenced. The circuit arrangement shown in Fig. 2 comprises only one switching element S. Means I for controlling the power consumed by the lamp La are formed by multiplier circuit 3 for generating a signal which is a measure for the power consumed by the lamp, and differential amplifier 4. Memory 7, light sensor SE, differential amplifier 5, and control circuit 2 form means III for controlling the luminous flux of the lamp. Timer circuit 6, switching element S, memory 7, differential amplifier 5, and light sensor SE form calibration means for automatic calibration of the means III in relation to the means I. Means IV for automatic activation of the means I after the run-up of the lamp are formed by timer circuit 6 and switching element S.

K1 and K2 are input terminals of ballast circuit VI for connection to a supply voltage source. The lamp La is coupled to output terminals of the ballast circuit VI. Inputs of the multiplier circuit 3 are coupled to the output terminals of the ballast circuit VI. An output of the multiplier circuit 3 is connected to switching element S. An output of timer circuit 6 is connected to a control electrode of switching element S and to a further input of memory 7. Switching element S is also connected to an input of differential amplifier 4. Switching element S can be in two alternative states: a first state and a second state. In the first state, switching element S breaks the connection between the output of multiplier circuit 3 and the input of differential amplifier 4, while in the second state the switching element S connects the output of multiplier circuit 3 to the input of differential amplifier 4. During operation of the circuit arrangement, a substan-

tially constant reference voltage, which is a measure for a desired value of the power consumed by the lamp, is present at a further input of differential amplifier 4. An output of differential amplifier 4 is connected to an input of memory 7. An output of memory 7 is connected to an input of differential amplifier 5. A further input of differential amplifier 5 is connected to an output of light sensor SE. An output of differential amplifier 5 is connected to an input of control circuit 2, and an output of control circuit 2 is connected to an input of the ballast circuit VI.

The operation of the circuit arrangement described is as follows.

If a supply voltage source is connected to the input terminals K1 and K2, the ballast circuit 1 during operation generates a current by which the lamp is operated. Immediately after the circuit arrangement has been made operational and the lamp has ignited, the switching element S is in the first state. As a result, the means I for controlling the power consumed by the lamp are not active, while the means III for controlling the luminous flux of the lamp are active. The luminous flux of the lamp immediately after ignition is lower than the desired value during a comparatively short initial phase. As is also indicated in the description of the operation of the circuit arrangement shown in Fig. 1, the circuit arrangement shown in Fig. 2 is provided with means, not shown, for preventing the lamp taking up an excessive power during this comparatively short initial phase. At the end of this comparatively short initial phase, the luminous flux of the lamp has risen to substantially the desired value. This desired value is determined by the signal present at the output of memory 7, which is a measure for the luminous flux of the lamp during stationary lamp operation. If the switching element S is in the first state, no signal is present at the input of memory 7. Memory 7 is then passive and keeps the value last stored. The signal at the output of memory 7 is compared with the signal at the output of the light sensor SE by differential amplifier 5. The signal at the output of differential amplifier 5 drives the control circuit 2. The control circuit 2 controls the power supplied to the lamp La by the ballast circuit in such a way that the luminous flux of the lamp remains constant.

A fixed time interval after lamp ignition, the timer circuit 6 switches the switching element S to the second state and at the same time activates the input of memory 7 through the further input of memory 7. The fixed time interval is chosen so as to be at least equal to the time duration required for the run-up of the lamp La in question. Both the means I for controlling the power consumed by the lamp and the means III for controlling the luminous flux of the lamp are active now. Since the reference voltage present at input 10 of differential amplifier 4 is substantially constant, while the contents of memory 7 are dependent on the signal at the output of differential amplifier 4, the means I are predominant over the means III, so that the combination of means I and III forms a control mechanism which keeps the pow-

er consumed by the lamp substantially constant. The signal at the output of memory 7 is continually adapted to the value of the signal at the output of the light sensor SE while the means I, means III, and the input of memory 7 are active. This means that a calibration of the means III in relation to the means I takes place continually during stationary lamp operation. This calibration achieves that the luminous flux of the lamp during the run-up is substantially equal to the luminous flux during stationary lamp operation, also in the case of ageing or pollution of the lamp or the light sensor.

In Fig. 3, input terminal 8 of the memory shown is connected to an input of sampling circuit 9. Reference numeral 14 denotes a further input of sampling circuit 9 for the activation of sampling circuit 9. An output of sampling circuit 9 is connected to an input of analog/digital converter 10. An output of analog/digital converter 10 is connected to an input of digital memory element 11. An output of digital memory element 11 is connected to an input of digital/analog converter 12. An output of digital/analog converter 12 is connected to output terminal 13 of the memory.

The operation of the memory shown is as follows.

If the memory is active, owing to the fact that the sampling circuit 9 is activated through further input 14, there is a connection between the input 8 and the output terminal of the sampling circuit 9, which connection is broken by the sampling circuit 9 with a sampling frequency f. As a result, the signal at the input of the analog/digital converter is replaced by the instantaneous value of the signal at input terminal 8 with a frequency f. The signal at the input of the analog/digital converter 10 is converted by the analog/digital converter 10 into a digital signal which is stored in the digital memory element 11. The digital signal is also present at the output of the digital memory element 11 and the input of digital/analog converter 12. The digital signal is converted into an analog signal by the digital/analog converter. The time interval during which the connection between input terminal 8 and the output of sampling circuit 9 is broken is chosen to be greater than the time interval required for digitizing the signal at the input of the analog/digital converter 10, storing it in digital form in the digital memory element 11, and adapting the signal at the output terminal 13. If the memory is passive, there is no connection between the input terminal 8 and the output of sampling circuit 9. In this passive state, the latest value of the digital signal, which was stored in the digital memory element 11 during the active state of the memory, is maintained in this memory element.

Claims

1. A circuit arrangement for operating a high-pressure discharge lamp provided with
 - a ballast circuit (VI) for generating a current

through the high-pressure discharge lamp from a supply voltage,

- first means (I) for controlling a power consumed by the high-pressure discharge lamp,
- second means (II) for influencing a run-up behaviour of the high-pressure discharge lamp and comprising third means (III) for controlling the luminous flux of the high-pressure discharge lamp,

characterized in that the third means (III) comprise a light sensor (SE) coupled with a control circuit (2) for controlling the power supplied to the high-pressure discharge lamp in such a way that the luminous flux of the high-pressure discharge lamp remains at a substantially constant level and in that the second means (II) further comprise fourth means (IV) for the automatic activation of the first means (I) after the run-up of the high-pressure discharge lamp.

2. A circuit arrangement as claimed in Claim 1, characterized in that the fourth means (IV) comprise a timer circuit for generating a signal after a fixed time interval after the ignition of the high-pressure discharge lamp.
3. A circuit arrangement as claimed in Claim 1 or 2, characterized in that the circuit arrangement is provided with calibration means for automatic calibration of the third means (III) in relation to the first means (I), and in that the third means (III) comprise a memory for storing a calibration signal which is a measure for the luminous flux of the high-pressure discharge lamp during stationary lamp operation.
4. A circuit arrangement as claimed in Claim 3, characterized in that the memory comprises a digital memory element, a digital/analog converter, and an analog/digital converter.

Patentansprüche

1. Schaltungsanordnung zum Betreiben einer Hochdruck-Entladungslampe mit
 - einer Vorschaltgerätschaltung (VI), um aus einer Speisespannung einen Strom durch die Hochdruck-Entladungslampe zu generieren,
 - ersten Mitteln (I) zum Steuern einer von der Hochdruck-Entladungslampe aufgenommenen Leistung,
 - zweiten Mitteln (II) zum Beeinflussen eines Hochlaufverhaltens der Hochdruck-Entladungslampe, und mit dritten Mitteln (III) zum Steuern des Lichtstroms der Hochdruck-Entladungslampe,

dadurch gekennzeichnet, daß die dritten Mittel (III) einen mit einer Steuerschaltung (2) gekoppelten Lichtsensor (SE) umfassen zum Steuern der von der Hochdruck-Entladungslampe aufgenommenen Leistung in der Weise, daß der Lichtstrom der Hochdruck-Entladungslampe auf nahezu konstantem Niveau bleibt, und daß die zweiten Mittel (II) weiterhin vierte Mittel (IV) zur automatischen Aktivierung der ersten Mittel (I) nach dem Hochlaufen der Hochdruck-Entladungslampe umfassen.

2. Schaltungsanordnung nach Anspruch 1, dadurch gekennzeichnet, daß die vierten Mittel (IV) eine Timer-Schaltung zum Generieren eines Signals nach einem festen Zeitintervall nach der Zündung der Hochdruck-Entladungslampe umfassen.
3. Schaltungsanordnung nach Anspruch 1 oder 2, dadurch gekennzeichnet, daß die Schaltungsanordnung mit Kalibrierungsmitteln zur automatischen Kalibrierung der dritten Mittel (III) bezüglich der ersten Mittel (I) versehen ist, und daß die dritten Mittel (III) einen Speicher zum Speichern eines Kalibrierungssignals umfassen, das ein Maß für den Lichtstrom der Hochdruck-Entladungslampe bei stationärem Lampenbetrieb ist.
4. Schaltungsanordnung nach Anspruch 3, dadurch gekennzeichnet, daß der Speicher ein digitales Speicherelement, einen Digital-Analog-Umsetzer, und einen Analog-Digital-Umsetzer umfaßt.

Revendications

1. Circuit de commutation pour faire fonctionner une lampe à décharge à haute pression comportant
 - un circuit de ballast (VI) pour engendrer d'une tension d'alimentation un courant traversant la lampe à décharge à haute pression,
 - des premiers moyens (I) pour commander une puissance consommée par la lampe à décharge à haute pression,
 - des deuxièmes moyens (II) pour influencer un comportement d'échauffement de la lampe à décharge à haute pression et comportant des troisièmes moyens (III) pour commander le flux lumineux de la lampe à décharge à haute pression,

caractérisé en ce que les troisièmes moyens (III) comportent un détecteur de lumière (SE) couplé à un circuit de commande (2) pour commander la puissance fournie à la lampe à décharge à haute pression de façon que le flux lumineux de la lampe à décharge à haute pression reste à un niveau sensiblement constant et en ce que les deuxièmes

moyens (II) comportent encore des quatrièmes moyens (IV) pour l'activation automatique des premiers moyens (I) après l'échauffement de la lampe à décharge à haute pression.

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2. Circuit de commutation selon la revendication 1, caractérisé en ce que les quatrièmes moyens (IV) comportent un circuit timer pour engendrer un signal après un intervalle de temps fixe après l'amorçage de la lampe à décharge à haute pression.

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3. Circuit de commutation selon la revendication 1 ou 2, caractérisé en ce que le circuit de commutation est muni de moyens de calibrage pour le calibrage automatique des troisièmes moyens (III) par rapport aux premiers moyens (I) et en ce que les troisièmes moyens (III) comportent une mémoire pour stocker un signal de calibrage étant une mesure pour le flux lumineux de la lampe à décharge à haute pression pendant le fonctionnement stationnaire de la lampe.

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4. Circuit de commutation selon la revendication 3, caractérisé en ce que la mémoire comporte un élément de mémoire numérique, un convertisseur numérique/analogique et un convertisseur analogique/numérique.

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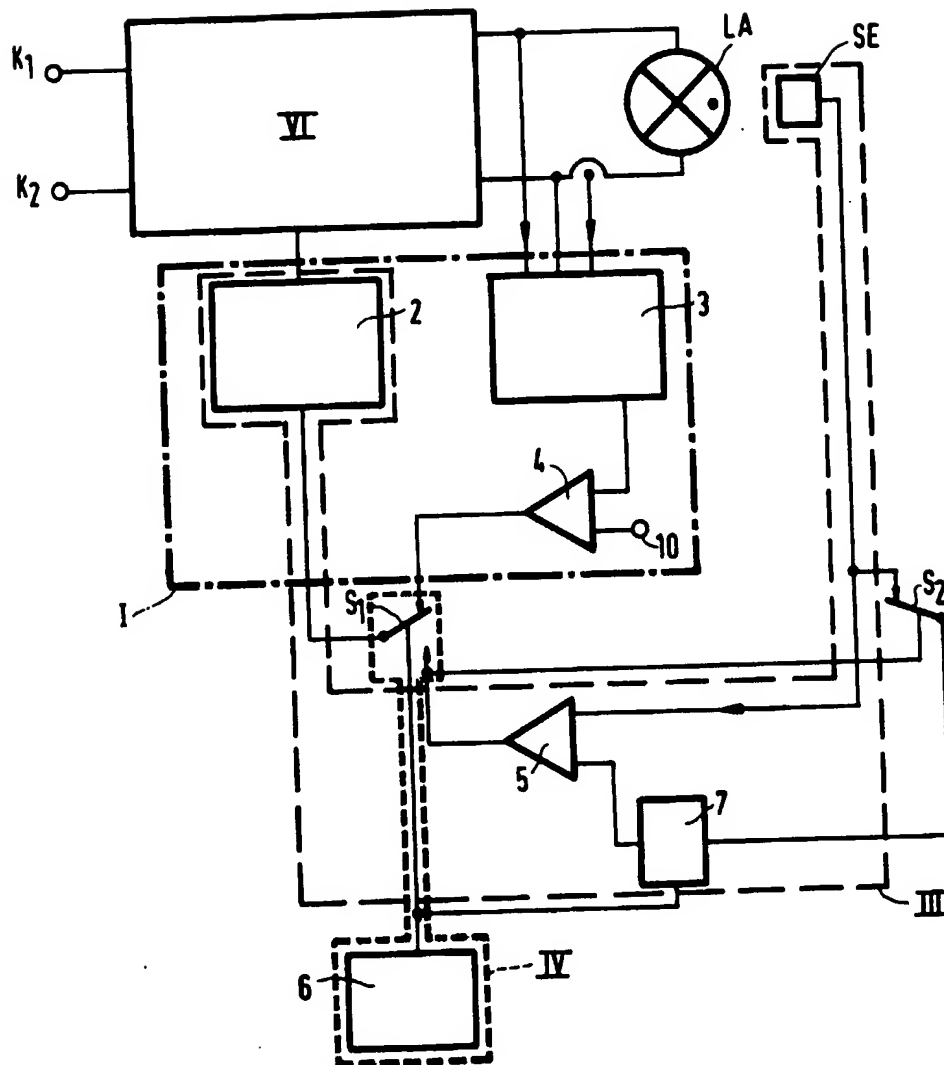
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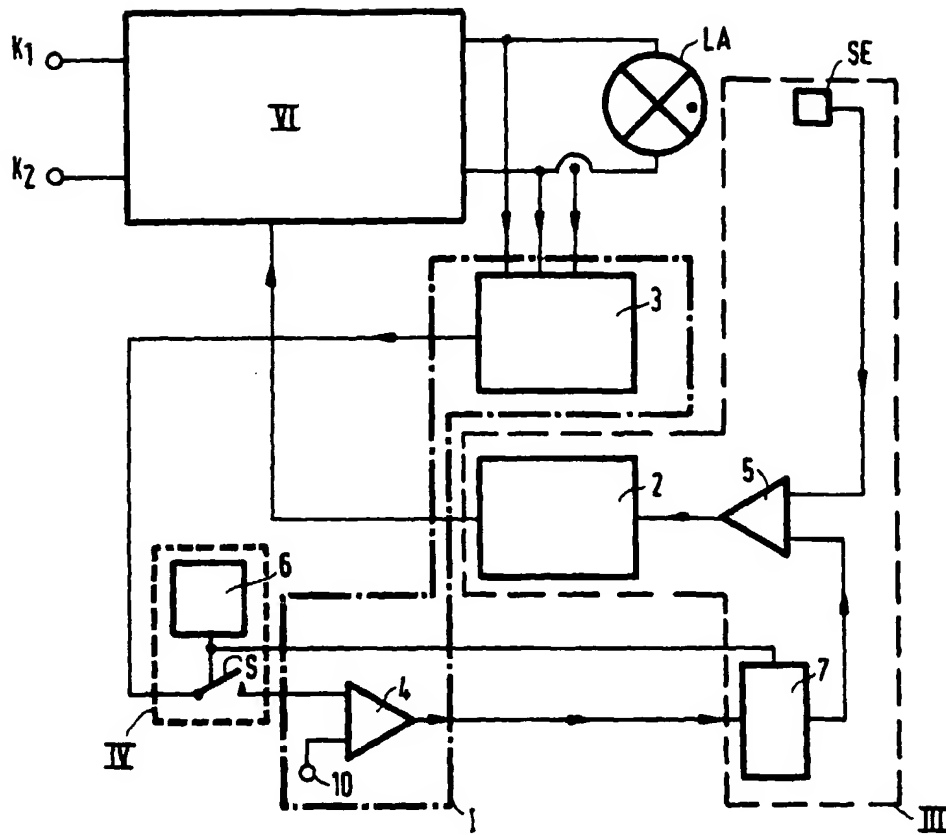


FIG. 2

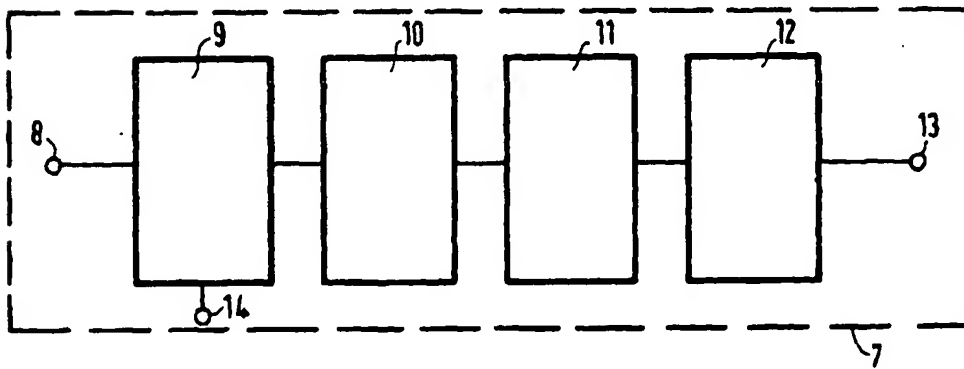


FIG. 3